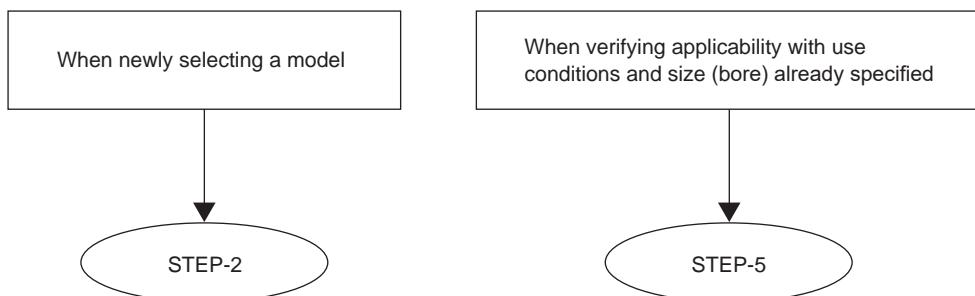


**MRG2 Series selection guide**

- As the selection conditions are different from those of general air cylinders, confirm whether the model is adequate or not according to selection guide.

**STEP-1****STEP-2**

- Confirming working conditions

1. Working pressure (P)	<input type="text"/> (MPa)
2. Applied load (W)	<input type="text"/> (N) (applied load = workpiece load + jig load)
3. Mounting orientation	Horizontal / vertical (Refer to Fig. 1 below)
4. Stroke (L)	<input type="text"/> (m)
5. Travel time (t)	<input type="text"/> (S)
6. Average speed (Va)	<input type="text"/> (m/s)

Formula for cylinder average speed Va

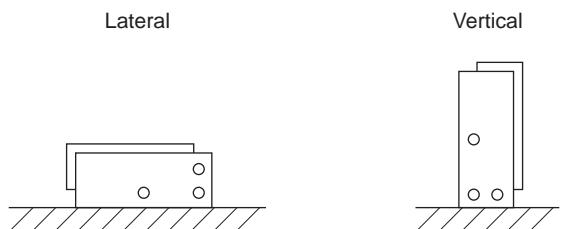
$$Va = \frac{L}{t} \text{ (m/s)}$$

[Mounting orientation]

Operating direction Horizontal, vertical - up, vertical - down

Mounting direction Lateral, vertical (refer to Fig. 1)

Fig. 1



SCP\*3

CMK2

CMA2

SCM

SCG

SCA2

SCS2

CKV2

CAV2/  
COVP/N2

SSD2

SSG

SSD

CAT

MDC2

MVC

SMG

MSD/  
MSDG

FC\*

STK

SRL3

SRG3

SRM3

SRT3

MRL2

MRG2

SM-25

ShkAbs

FJ

FK

Spd  
Contr

Ending

## STEP-3

### ● Calculation of required thrust

Calculate the required thrust ( $F_N$ ) of the cylinder.

1. For horizontal operation

$$F_N = W \times 0.2^* = \boxed{\quad} \text{ (N)}$$

2. For vertical operation

$$F_N = W = \boxed{\quad} \text{ (N)}$$

\* This is the frictional resistance value of the guide, etc., when a load is placed on the slider. Consider separately when there is further external resistance.

## STEP-4

### ● Selection of approximate size of cylinder

$\text{Required thrust of cylinder } F_N \leq \text{theoretical thrust} \times \frac{\mu}{100} \times \frac{\alpha}{100}$
---

$\mu$ : Thrust efficiency (%) (refer to Fig. 2.)

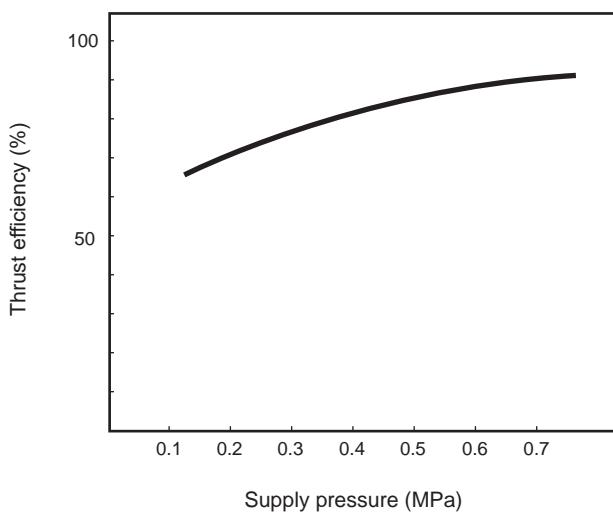
$\alpha$ : Load factor (%) (refer to Fig. 2.)

Select a cylinder size which satisfies this condition.

Table 1. Theoretical thrust value

Bore size (mm)	Working pressure MPa						(N)
	0.2	0.3	0.4	0.5	0.6	0.7	
ø10	-	24	31	39	47	55	
ø16	40	60	80	101	121	141	
ø25	98	147	196	245	295	344	

Fig. 2 Thrust efficiency  $\mu$



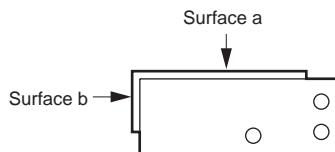
Load factor  $\alpha$ : For general use, the value within the range in Table 2 is desirable.

Table 2. Load factor guidelines

Working pressure MPa	$\alpha$ (%)
0.2 to 0.3	$\alpha \leq 40$
0.3 to 0.6	$\alpha \leq 50$
0.6 to 0.7	$\alpha \leq 60$

**STEP-5****● Calculate the vertical load and value for each moment**

Calculate the vertical loads ( $W_1$ ,  $W_2$ ) and the moments ( $M_1$ ,  $M_2$ ,  $M_3$ ) depending on the load cylinder mounting status.



	Mounting on surface a	Mounting on surface b	Calculation results
Vertical load $W_1$ $W_2$			$W_1 = \boxed{\phantom{000}}$ $W_2 = \boxed{\phantom{000}}$
Bending moment $M_1 = F_1 \times l_1$	<p><math>l_1</math></p> <p><math>F_1</math></p> <p><math>X</math> is the distance from the surface of the slider to the working point of the force</p>	<p><math>l_1</math></p> <p><math>F_1</math></p>	$M_1 = \boxed{\phantom{000}}$
Radial moment $M_2 = F_2 \times l_2$	<p><math>C.L</math></p> <p><math>l_2</math></p> <p><math>F_2</math></p> <p><math>l_2 = X + C</math></p> <p><math>C.L</math> indicates the center point between the set screws on surface a</p>	<p><math>C.L</math></p> <p><math>l_2</math></p> <p><math>F_2</math></p> <p><math>l_2 = X + C</math></p> <p><math>l_2 = X + D</math></p>	$M_2 = \boxed{\phantom{000}}$
Torsion moment $M_3 = F_3 \times l_3$	<p><math>l_3</math></p> <p><math>F_3</math></p>	<p><math>l_3</math></p> <p><math>F_3</math></p> <p><math>l_3 = X + C</math></p> <p><math>l_3 = X + D</math></p>	$M_3 = \boxed{\phantom{000}}$

Table 3. Values of each parameter

Bore size (mm)	C	D
ø10	0.016	0.012
ø16	0.020	0.014
ø25	0.026	0.020

- SCP\*3
- CMK2
- CMA2
- SCM
- SCG
- SCA2
- SCS2
- CKV2
- CAV2/  
COVP/N2
- SSD2
- SSG
- SSD
- CAT
- MDC2
- MVC
- SMG
- MSD/  
MSDG
- FC\*
- STK
- SRL3
- SRG3
- SRM3
- SRT3
- MRL2
- MRG2**
- SM-25
- ShkAbs
- FJ
- FK
- Spd  
Contr
- Ending

SCP\*3

CMK2

CMA2

SCM

SCG

SCA2

SCS2

CKV2

CAV2/  
COVP/N2

SSD2

SSG

SSD

CAT

MDC2

MVC

SMG

MSD/  
MSDG

FC\*

STK

SRL3

SRG3

SRM3

SRT3

MRL2

MRG2

SM-25

ShkAbs

FJ

FK

Spd  
Contr

Ending

## STEP-6

### ● Confirmation of the vertical load and the composite value for each moment

Divide each load with the max. allowable values listed in Table 4 and confirm that the total value thereof is 1.0 or less.

$$\frac{W_1 \text{ (or } W_2)}{W_1 \text{ (or } W_2) \text{ max}} + \frac{M_1}{M_{1\max}} + \frac{M_2}{M_{2\max}} + \frac{M_3}{M_{3\max}} \leq 1.0$$

When the total value is greater than 1.0

1. Review the load → STEP-2
2. Use a cylinder with wider bore size, etc., for revision. → Increase cylinder bore size  
→ STEP-5

Table 4. Max. allowable values of vertical load and moments

Bore size (mm)	W1max(N)	W2max(N)	M1max (N·m)	M2max (N·m)	M3max (N·m)
ø10	44	35	2.2	1.2	2.2
ø16	103	91	7.4	3.2	7.4
ø25	176	176	18.3	7.3	18.3

## STEP-7

### ● Confirmation of kinetic energy

Calculate the kinetic energy from load weight m (kg) and speed V (m/s) to confirm that the value is within the range of the specifications of the shock absorber. If the kinetic energy exceeds the specifications, increase the cylinder size or install an external shock absorber.

#### (1) Formula for kinetic energy calculation

$$E_1 = \frac{1}{2} \times m \times V^2 = \boxed{\quad} \text{ (J)}$$

E<sub>1</sub> : Kinetic energy (J)

m : Load weight (kg)

V : Speed (m/s)

W : Applied load (N)

L : Cylinder stroke (m)

t : Operating time (s)

α : Cylinder load factor (%)

F<sub>N</sub> : Required thrust (N)

μ : Thrust efficiency (%)

$$m = \frac{W}{9.8} = \boxed{\quad} \text{ (kg)}$$

$$V = \frac{L}{t} \times \left[ 1 + 1.5 \times \frac{\alpha}{100} \right] = \boxed{\quad} \text{ (m/s)}$$

$$\alpha = \frac{F_N}{\text{Cylinder theoretical thrust} \times \frac{\mu}{100}} \times 100 = \boxed{\quad} \text{ (%)}$$

#### (2) Shock absorber

The shock absorber used with MRG2 is shown in Table 5.

Table 5. Shock absorber specifications

Model	MRG2-10	MRG2-16	MRG2-25
Shock absorber model No.	MRG2-10-C (NCK-00-0.3 used)	MRG2-16-C (NCK-00-0.7 used)	MRG2-25-C (NCK-00-1.2 used)
Max. absorbed energy (J) <sup>1)</sup>	2.1	5.3	8.7
Stroke (mm) <sup>1)</sup>	5	7	8.5
Absorbed energy per hour (kJ/hour)	6.3	12.6	21.6
Max. operating frequency (cycle/min)	35	30	30

<sup>1)</sup> As a stopper cap is used to stop the piston before the stroke end, the energy and stroke are both smaller than standard products.

### ● Confirmation of allowable colliding energy of shock absorber

Calculate colliding object equivalent weight  $M_e$  and colliding energy  $E$  with the formula listed in the table below and confirm that  $M_e$  and  $E$  are less than or equal to the allowable values listed in Fig. 4 and Table 5. Also confirm that the repetition frequency is less than or equal to the allowable value according to Table 5.

### ● Code

$E$ : Colliding energy	<input type="text"/> (J)
$M_e$ : Colliding object equivalent weight	<input type="text"/> (kg)
$m$ : Load weight	<input type="text"/> (kg)
$F$ : Cylinder thrust	<input type="text"/> (N)
$V$ : Colliding speed	<input type="text"/> (m/s)
$St$ : Shock absorber stroke	<input type="text"/> (m)
$g$ : Gravity acceleration	9.8 (m/s <sup>2</sup> )

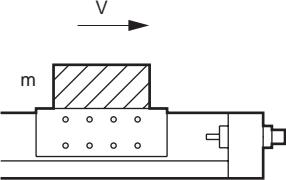
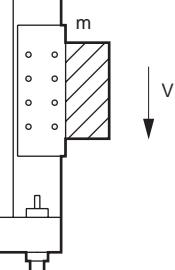
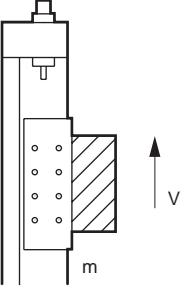
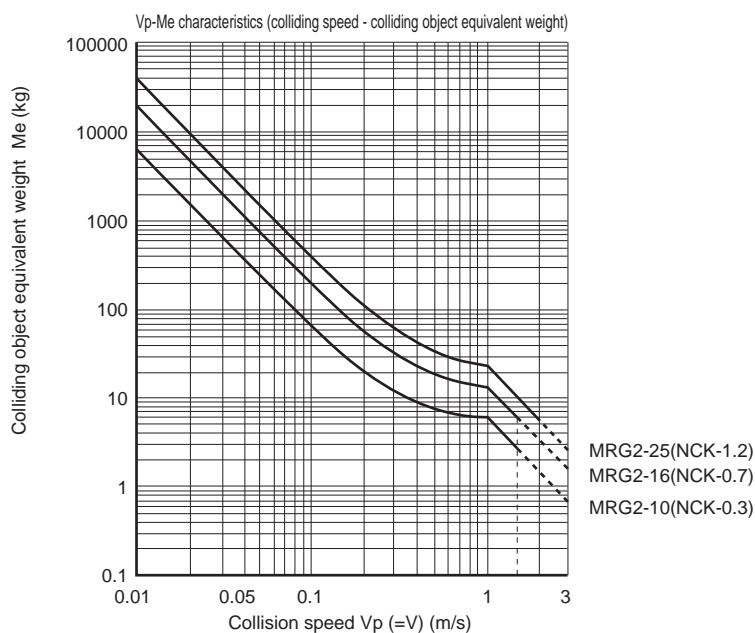
	Horizontal movement	Vertical down	Vertical up
Applications			
Colliding object equivalent weight $M_e$ (kg)	$M_e = m + \frac{2F \cdot St}{V^2}$	$M_e = m + \frac{2 \cdot St (F+mg)}{V^2}$	$M_e = m + \frac{2 \cdot St (F-mg)}{V^2}$
Energy $E$ (J)	$E = \frac{mV^2}{2} + F \cdot St$	$E = \frac{mV^2}{2} + (F+mg) \cdot St$	$E = \frac{mV^2}{2} + (F-mg) \cdot St$

Fig. 4



- SCP\*3
- CMK2
- CMA2
- SCM
- SCG
- SCA2
- SCS2
- CKV2
- CAV2/  
COVP/N2
- SSD2
- SSG
- SSD
- CAT
- MDC2
- MVC
- SMG
- MSD/  
MSDG
- FC\*
- STK
- SRL3
- SRG3
- SRM3
- SRT3
- MRL2
- MRG2**
- SM-25
- ShkAbs
- FJ
- FK
- Spd Contr
- Ending

## STEP-8

### ● Confirmation of inertia load

Inertia force functioning due to the load will operate at the end of the stroke.

Confirm whether this force is within the allowable range.

(1) Calculate inertia force  $F_i$  according to speed  $V$  and the inertia force coefficient shown in Fig. 5.

$$F_i = 9.8 \times m \times G(N)$$

$m$ : Load weight (kg)

$G$ : Inertia force coefficient

(2) Calculate the moment and load that is generated due to the inertia force.

(Example)

$$M_{1i} = F_i \times l_1$$

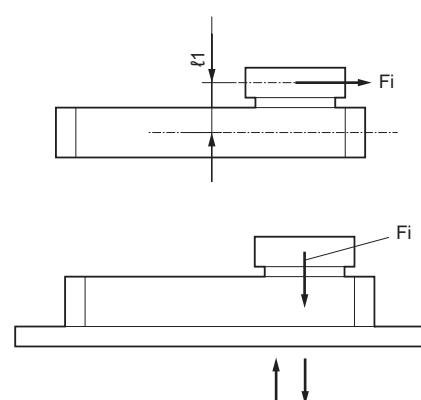
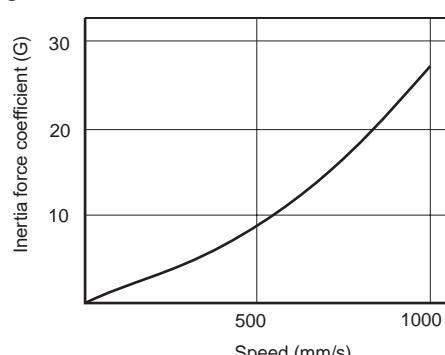


Fig. 5. Inertia force coefficient



(3) Add the load and moment generated by static load and inertial force, divide each load with the allowable values listed in Table 4 and confirm that the total values thereof are 1.0 or less.

$$W_{1g} = W_1 + W_{1i}$$

$$M_{1g} = M_1 + M_{1i}$$

$$W_{2g} = W_2 + W_{2i}$$

$$M_{2g} = M_2 + M_{2i}$$

$$M_{3g} = M_3 + M_{3i}$$

$$\frac{W_{1g} (\text{or } W_{2g})}{W_1 (\text{or } W_2) \text{ max}} + \frac{M_{1g}}{M_1 \text{ max}} + \frac{M_{2g}}{M_2 \text{ max}} + \frac{M_{3g}}{M_3 \text{ max}} \leq 1.0$$

When vertically moving the entire cylinder

SCP\*3

CMK2

CMA2

SCM

SCG

SCA2

SCS2

CKV2

CAV2/  
COVP/N2

SSD2

SSG

SSD

CAT

MDC2

MVC

SMG

MSD/  
MSDG

FC\*

STK

SRL3

SRG3

SRM3

SRT3

MRL2

MRG2

SM-25

ShkAbs

FJ

FK

Spd  
Contr

Ending