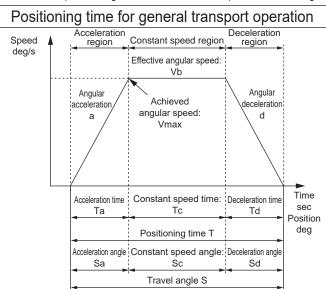
Calculate the positioning time with the selected product according to the following example and confirm that the required tact is attainable.



Set value	Set angular speed	V	deg/s		
	Set angular acceleration	а	deg/s ²		
Set value	Set angular deceleration	d	deg/s ²		
	Travel angle	S	deg		
	Achieved angular speed	Vmax	deg/s	$= \{2 \times a \times d \times S/(a + d)\}^{1/2}$	
	Effective angular speed	Vb	deg/s	The lesser value of V and Vmax	
	Acceleration time	Ta	s	= Vb/a	
0-11-41	Deceleration time	Td	S	= Vb/d	
Calculated value	Constant speed time	Tc	S	= Sc/Vb	
value	Acceleration angle	Sa	deg	$= (a \times Ta^2)/2$	
	Deceleration angle	Sd	deg	$= (d \times Td^2)/2$	
	Constant speed angle	Sc	deg	= S - (Sa + Sd)	
	Positioning time	Т	S	= Ta + Tc + Td	
* Do not use at angular speeds that exceed the specifications					

- Do not use at angular speeds that exceed the specifications. Depending on angular acceleration/deceleration and travel angle, the trapezoid speed waveform may not be formed (the set angular speed may not be achieved).
- In this case, select the effective angular speed (Vb) from the set angular speed (V) and the achieved angular speed (Vmax), whichever is smaller. Use at the angular acceleration/angular deceleration of 3000 deg/s² or less. While settling time depends on working conditions, it may take 0.2 seconds or so.

- 1G≒9800deg/s

Positioning time for pressing operation						
Angular A	A	cceleratio	on Constant speed D	eceleration region	n	_
speed deg/s			Effective angular speed: Vb	Angular		
		Angular acceleration a	Achieved angular speed: Vmax	deceleration d	Pressing speed Vn	
		Acceleration time	Constant speed time: Tc	Deceleration time Td	Pressing time Tn	Time
			Positioning time T			Position deg
		Acceleration angle Sa	Constant speed angle: Sc	Deceleration angle Sd	Pressing angle Sn	
			Travel angle S	3		

	Item	Code	Unit	Remarks
	Set angular speed	V	deg/s	
	Set angular acceleration	а	deg/s ²	
Set value	Set angular deceleration	d	deg/s ²	
Set value	Travel angle	S	deg	
	Pressing speed	Vn	deg/s	
	Pressing angle	Sn	deg	
	Achieved angular speed	Vmax	deg/s	$= \{2 \times a \times d \times (S - Sn + Vn^2/2/d)/(a + d)\}^{1/2}$
	Effective angular speed	Vb	deg/s	The lesser value of V and Vmax
	Acceleration time	Ta	S	= Vb/a
	Deceleration time	Td	S	= (Vb - Vn)/d
Calculated	Constant speed time	Tc	S	= Sc/Vb
value	Pressing time	Tn	S	= Sn/Vn
	Acceleration angle	Sa	deg	$= (a \times Ta^2)/2$
	Deceleration angle	Sd	deg	$= ((Vb + Vn) \times Td)/2$
	Constant speed angle	Sc	deg	= S - (Sa + Sd + Sn)
	Positioning time	Т	s	= Ta + Tc + Td + Tn

- Do not use at angular speeds that exceed the specifications.
- Depending on angular acceleration/deceleration and travel angle, the trapezoid speed waveform may not be formed (the set angular speed may not be achieved). In this case, select the effective angular speed (Vb) from the set angular
- speed (V) and the achieved angular speed (Vmax), whichever is smaller. Use at the angular acceleration/angular deceleration of 3000 deg/s² or less.
- * Use at the angular acceleration/angular deceleration of cools day, of the settling time depends on working conditions, it may take 0.2 seconds or so.

 * 1G≒9800deg/s²

Confirming load moment of inertia

Calculate the load moment of inertia, and then select a model from the angular speed and allowable moment of inertia graph.

2	Shape	Sketch	Requirements	Moment of inertia I kg·m²	Radius of rotation
precaul	Dial plate	d	● Diameter d (m) ● Weight M (kg)	$I=\frac{Md^2}{8}$	$\frac{d^2}{8}$
	Thin rectangle plate (rectangular parallelepiped)	a ₂ a ₁ b	●Plate length a ₁ a ₂ ●Side length b ●Weight M ₁	$I = \frac{M_1}{12} (4a_1^2 + b^2) + \frac{M_2}{12} (4a_2^2 + b^2)$	$\frac{(4a_1^2 + b^2) + (4a_2^2 + b^2)}{12}$

[At 24 VDC] Angular speed and Allowable moment of inertia (kg·m²) allowable moment of inertia [Example: FGRC-30] 0.020 0.015 0.010 0.005 0.000 100 150 Angular speed (deg/s)

*Refer to pages 30, 32 and 34.

I L

FLCR

FGRC

ECZ

(controller)

Salety

STEP 3 Confirming required torque

Use the following equations to determine the maximum load torque, and then refer to the angular speed and output torque graph to select the applicable model.

Selection method is roughly categorized into three load types.

In each case, the required torque must be calculated. If the load is a compound load, add each torque to calculate the required torque.

[At 48 VDC]

5.0

4.0 3.0

2.0

1.0

0.0 |

[At 24 VDC]

5.0

4.0

3.0

2.0

1.0

0.0

0

50

Output torque (N·m)

Output torque (N·m)

Angular speed and output torque

Angular speed (deg/s)

100

100

FGRC-50

FGRC-30

FGRC-10

300

FGRC-50

FGRC-30

FGRC-10

250

200

200

Angular speed and output torque

150

Angular speed (deg/s)

(1) Static load (Ts)

When static pushing force is required for clamp, etc.

 $Ts=Fs \times L$

Ts: Required torque (N·m)

Fs: Required force (N)

L: Length from center of rotation to pressure cone apex (m)

(2) Resistance load (TR)

When force including frictional force, gravity or other external force is applied

$$T_R=3 \times F_R \times L$$

TR: Required torque (N·m)

FR: Required force (N)

L: Length from center of rotation to pressure cone apex (m)

(3) Inertia load (TA)

When the object is rotated

$$T_A=3\times I\times\dot{\omega}$$

TA: Required torque (N·m)

I: Moment of inertia (kg·m²)

ώ: Set angular acceleration/deceleration (rad/s²)

θ: Travel angle (rad)

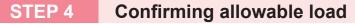
t: Travel time (s)

* Calculate $\dot{\omega}$ from angular acceleration or angular deceleration, whichever is higher.

The formula below can be used to determine the radian (rad) from the degree (deg).

 $rad = deg x (\pi/180)$

Use the moment of inertia and travel time (pages 30, 32, and 34) or the figure for moment of inertia calculation (page 43) to calculate the moment of inertia.



If load applies to table, load is to be within allowable value on Table 1.

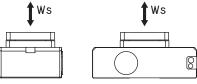
For combined multiple load, ensure that the total is 1.0 or less.

Table 1

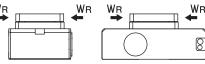
Model No.	W _s max	W _R max	M max
FGRC-10	80	80	2.5
FGRC-30	200	200	5.5
FGRC-50	450	320	10

W_S : Thrust load (N)
W_R : Radial load (N)
M : Moment load (N⋅m)
W_{Smax} : Allowable thrust load (N)
W_{Rmax} : Allowable radial load (N)
M_{max} : Allowable moment load (N⋅m)

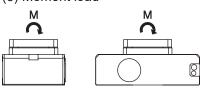
(1) Thrust load (axial load)



(2) Radial load (lateral load)

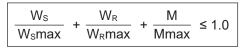


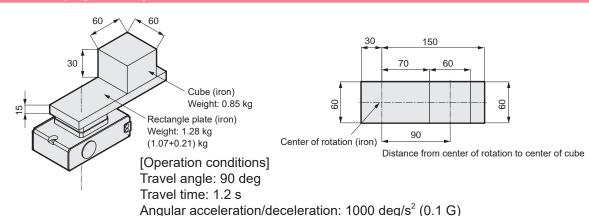
(3) Moment load



Combined load

Substitute the result to the following formula, and check after each load is calculated.





STEP 1 Confirming positioning time

Positioning time is 1.09 s according to operation conditions. This is lower than the required travel time of 1.2 s, so proceed to the next step.

Set value

Angular speed	V	90 deg/s
Angular acceleration	а	1000 deg/s ²
Angular deceleration	d	1000 deg/s ²
Travel angle	S	90 deg

Calculated value

Achieved angular speed	Vmax	300 deg/s
Effective angular speed	Vb	90 deg/s
Acceleration time	Та	0.09 s
Deceleration time	Td	0.09 s
Constant speed time	Tc	0.91 s
Positioning time	Т	1.09 s

STEP 2 Confirming load moment of inertia

Calculate the moment of inertia I, and then temporarily select a model from the angular speed and allowable moment of inertia graph.

[Rectangle plate]

$$11 = 1.07 \times \frac{4 \times 0.15^2 + 0.06^2}{12} + 0.21 \times \frac{4 \times 0.03^2 + 0.06^2}{12} = 0.00847$$

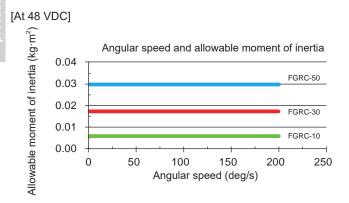
Cube

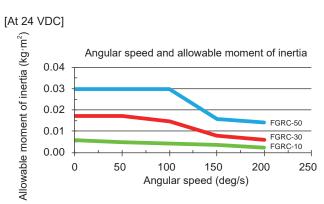
$$12 = 0.85 \times \left[\frac{0.06^2 + 0.06^2}{12} + 0.09^2 \right] = 0.00740$$

The overall moment of inertia I is as follows.

$$I = I1 + I2 = 0.01587 (kg \cdot m^2).....(1)$$

From the graph of angular speed and allowable moment of inertia, select FGRC-30 [48 VDC], which satisfies the allowable moment of inertia at angular speed 90 deg/s.





STEP 3 Confirming required torque

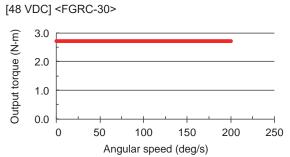
Calculate the load torque and confirm that it is within the range in the graph of angular speed and output torque. Set acceleration/deceleration from $a=d=1000 \text{ deg/s}^2$

$$\dot{\omega} = 1000 \times \frac{\pi}{180}$$
= 17.45 rad/s²(2)

From (1) and (2), inertia load (T_A) is

$$T_A = 3 \times 0.01587 \times 17.45$$

= 0.831 (N·m)



The intersection of angular speed V = 90 (deg/s) and $T_A = 0.598$ (N·m) is toward the interior of the graph, meaning use is possible.

STEP 4 Confirming allowable load

Finally, check if value is within allowable load range after load value that applies to table is calculated.

[Thrust load] The total weight is 1.07 + 0.21 + 0.85 = 2.13 (kg) Therefore, the thrust load (Ws) is Ws = $2.13 \times 9.8 = 20.9$ (N)

[Radial load] Since no radial load is applied, WR = 0 (N)

[Moment load] The moment load from the rectangle plate (M₁) is $1.07 \times 9.8 = 10.5$ (N) $0.21 \times 9.8 = 2.06$ (N) Therefore, M₁ = $10.5 \times 0.075 - 2.06 \times 0.015 = 0.76$ (N·m)

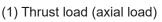
The moment load from the rectangular parallelepiped (M₂) is $0.85 \times 9.8 = 8.3$ (N) Therefore, $M_2 = 8.3 \times 0.09 = 0.75$ (N·m)

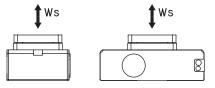
When M₁ and M₂ are totaled, M= 0.76 + 0.75 = 1.51 (N·m)

$$\frac{\text{Ws}}{\text{Wsmax}} + \frac{\text{WR}}{\text{WRmax}} + \frac{\text{M}}{\text{Mmax}}$$

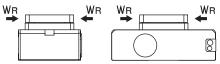
$$\frac{20.9}{200} + \frac{0}{200} + \frac{1.51}{5.5} = 0.4 \le 1.0$$

The total load value is within the allowable load value, so FGRC-30 can be selected.

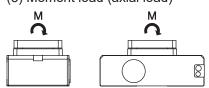




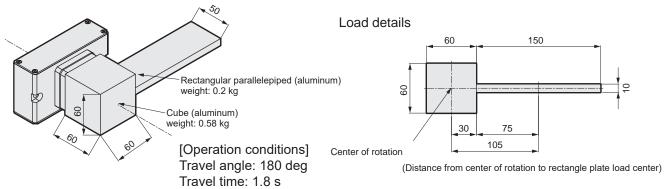
(2) Radial load (axial load)



(3) Moment load (axial load)



Selection example [Wall-mounted



Angular acceleration/deceleration: 1000 deg/s² (0.1 G)

STEP 1 Confirming positioning time

Positioning time is 1.57 s according to operation conditions.

This is lower than the required travel time of 1.8 s, so proceed to the next step.

Set value

Angular speed	V	125 deg/s
Angular acceleration	а	1000 deg/s ²
Angular deceleration	d	1000 deg/s ²
Travel angle	S	180 deg

Calculated value

Achieved angular speed	Vmax	424.3 deg/s
Effective angular speed	Vb	125 deg/s
Acceleration time	Ta	0.125 s
Deceleration time	Td	0.125 s
Constant speed time	Tc	1.315 s
Positioning time	Т	1.57 s

STEP 2 Confirming load moment of inertia

Calculate the moment of inertia I, and then temporarily select a model from the angular speed and allowable moment of inertia graph.

[Rectangular parallelepiped]

$$I_1 = 0.2 \times \frac{(0.01^2 + 0.15^2)}{12} + 0.2 \times 0.105^2 = 0.00258 \text{ (kg} \cdot \text{m}^2\text{)}$$

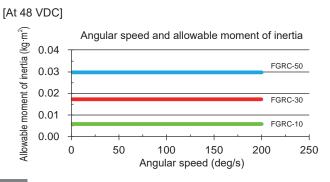
[Cube]

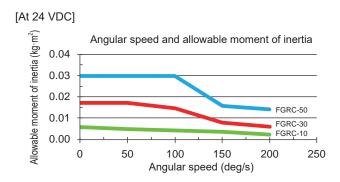
$$I_2 = 0.58 \times \frac{(0.06^2 + 0.06^2)}{12} = 0.00035 \text{ (kg} \cdot \text{m}^2\text{)}$$

Therefore, the overall moment of inertia is as follows.

$$I = I_1 + I_2 = 0.00293 \text{ (kg} \cdot \text{m}^2)...... (1)$$

From the graph of angular speed and allowable moment of inertia, select FGRC-10 [48 VDC], which satisfies the allowable moment of inertia at angular speed 125 deg/s.





STEP 3 Confirming required torque

Calculate the load torque and confirm that it is within the range in the graph of angular speed and output torque. Calculate the load torque using the gravitational resistance load (TR) and inertia load (TA).

[Resistance load]

$$TR = 3 \times 0.2 \times 9.8 \times 0.105$$

= 0.617 (N·m)(2)

[Inertia load]

Set acceleration/deceleration from $a = d = 1000 \text{ deg/s}^2$

$$\dot{\omega} = 1000 \times \frac{\pi}{180}$$

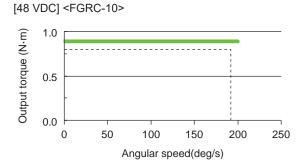
$$= 17.45 \text{ rad/s}^2 \dots (3)$$

From (1) and (3), inertia load (T_A) is

$$T_A = 3 \times 0.00293 \times 17.45$$

= 0.153 (N·m)(4)

From (2) and (4), total load torque (T) is
$$T = TR + TA = 0.617 + 0.153 = 0.77 \text{ (N·m)}$$



The intersection of angular speed V=180(deg/s) and T=0.77(N·m) is toward the interior of the graph, meaning use is possible.

Confirming allowable load STEP 4

Finally, check if value is within allowable load range after load value that applies to table is calculated.

[Thrust load]

Since no thrust load is applied,

$$Ws = 0 (N)$$

[Radial load]

The total weight is

$$0.2 + 0.58 = 0.78(kg)$$

Therefore, the radial load (WR) is

$$WR = 0.78 \times 9.8 = 7.64(N)$$

[Moment load]

Based on the figure to the lower right, the moment load (M) is

 $M = 0.03 \times (0.2 + 0.58) \times 9.8 = 0.23 (N \cdot m)$

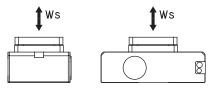
Therefore,

$$\frac{\text{WS}}{\text{WSmax}} + \frac{\text{WR}}{\text{WRmax}} + \frac{\text{M}}{\text{Mmax}}$$

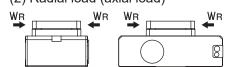
$$\frac{0}{80} + \frac{7.64}{80} + \frac{0.23}{2.5} = 0.19 \le 1.0$$

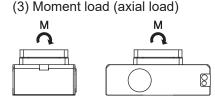
Therefore, the total load value is within the total allowable load, so FGRC-10 can be selected.

(1) Thrust load (axial load)



(2) Radial load (axial load)





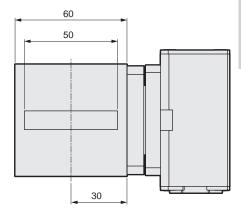
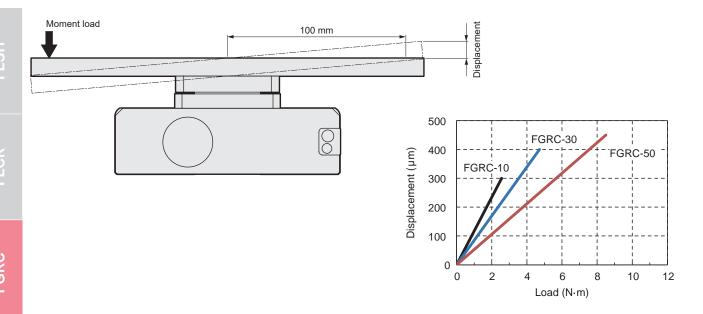
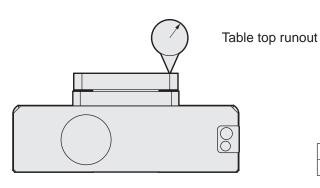


Table deflection at 100 mm away from center of rotation when moment load is applied to FGRC. (It is assumed that the table is in a non-rotating stationary state.)

Table deflection



Deflection: Displacement during 180° travel *Reference value



(mm)

Measurement location FGRC

Table top runout 0.1

Figure for moment of inertia calculation

d)	When rotary shaft passes through the workpiece						
Shape	Sketch	Requirements	Moment of inertia I kg·m²	Radius of rotation K ₁ ²	Remarks		
Dial plate		Diameter d(m)Weight M(kg)	$I = \frac{Md^2}{8}$	$\frac{d^2}{8}$	 No mounting direction For sliding use, contact CKD. 		
Stepped dial plate	d_1 d_2	● Diameter d₁(m) d₂(m) ● Weight d₁ section M₁(kg) d₂ section M₂(kg)	$I = \frac{1}{8} \left(M_1 d_1^2 + M_2 d_2^2 \right)$	$\frac{d_1^2 + d_2^2}{8}$	● Ignore when the d₂ section is extremely small compared to the d₁ section		
Bar (center of rotation at end)		■ Bar length R(m)■ Weight M(kg)	$I = \frac{MR^2}{3}$	$\frac{R^2}{3}$	 Mounting direction is horizontal Oscillating time changes when the mounting direction is vertical 		
Thin rod	R ₂	● Bar length R ₁ R ₂ ● Weight M ₁ M ₂	$I = \frac{M_1/R_1^2}{3} + \frac{M_2/R_2^2}{3}$	$\frac{R_1^2 + R_2^2}{3}$	 Mounting direction is horizontal Oscillating time changes when the mounting direction is vertical 		
in rectangle plate igular parallelepiped) (center of rotation at center of gravity)	R	● Bar length R (m)● Weight M(kg)	$I = \frac{MR^2}{12}$	R ² 12	No mounting direction		
Thin rectangle plate (rectangular parallelepiped)	a ₂ b	 Plate length Side length Weight M1 M2 	$I = \frac{M_1}{12} (4a_1^2 + b^2) + \frac{M_2}{12} (4a_2^2 + b^2)$	$\frac{(4a_1^2 + b^2) + (4a_2^2 + b^2)}{12}$	 Mounting direction is horizontal Oscillating time changes when the mounting direction is vertical 		
Rectangular parallelepiped	a	● Side length a(m) b(m) ● Weight M(kg)	$I = \frac{M}{12} (a^2 + b^2)$	$\frac{a^2 + b^2}{12}$	 No mounting direction For sliding use, contact CKD. 		
Concentrated load	Arm M ₂	● Shape of concentrated load ● Length to center of gravity of concentrated load R₁ ● Arm length R₂(m) ● Concentrated load weight M₁(kg) ● Arm weight M₂(kg)	$I = M_1 (R_1^2 + k_1^2) + \frac{M_2 R_2^2}{3}$	Calculate k ₁ ² according to shape of concentrated load	 Mounting direction is horizontal When M2 is extremely small compared to M1, it may be calculated as M2 = 0 		
How to	convert load J∟ to rotary actuat	or shaft rotation when using w	vith gear	I			
ar	Load IL	Gear Rotary side (No. of teeth) a Load side (No. of teeth) b	Load moment of inertia for the rotary actuator's shaft rotation		When gear shape is larger, gear moment of inertia		

 $IH = \left(\frac{a}{b}\right)^2 IL$

Load

moment of inertia

 $N \cdot m$

Rotary

should be

considered.

moment of inertia

Rotary shaft offsets from workpiece

	ary snart offsets from workpiece			
Shape	Sketch	Requirements	Moment of inertia l kg⋅m²	Remarks
Rectangular parallelepiped	R	● Side length a(m)	$I = \frac{M}{12} (a^2 + b^2) + MR^2$	● Same for cube
Hollow rectangular parallelepiped	R h ₁ h ₂	● Side length h₁(m) h₂(m) ● Distance from rotary shaft to load center R(m) M(kg)	$I = \frac{M}{12} (h_1^2 + h_2^2) + MR^2$	Cross section is for cube only
Cylinder	R	 Diameter d(m) Distance from rotary shaft to load center N(m) Weight M(kg) 	$I = \frac{Md^2}{16} + MR^2$	
Hollow cylinder	R	● Diameter d₁(m) d₂(m) ● Distance from rotary shaft to load center R(m) ● Weight M(kg)	$I = \frac{M}{16} (d_1^2 + d_2^2) + MR^2$	

^{*} To find moment of inertia, first convert load, jig, etc., to simple shapes with modeling, then calculate values. For the combined load, calculate each inertial moment and their total.